

FAA/EASA Composite Transport Workshop on Fatigue, Damage Tolerance, Maintenance and Crashworthiness



17th to 19th of May 2011, Atlanta

LEF factors and composite/metal fatigue LARGE SCALE COMPOSITE FATIGUE TEST PROTOCOL

Presented by

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Content

Hybrid Fatigue full scale Cells ?

- Needs of hybrid cells
- Metallic and Composite test scenarios

LEF definition

- Initial approach: Northrop
- Other analyses
- LEF trends versus scatter analysis

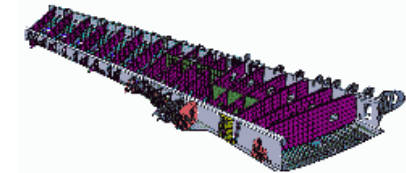
Perspectives

Hybrid Fatigue Full scale Cells ?

➔ Needs of Hybrid fatigue Cell:

- More and more hybrid structures: A320 ~10%, A380 ~30% A350 ~50%

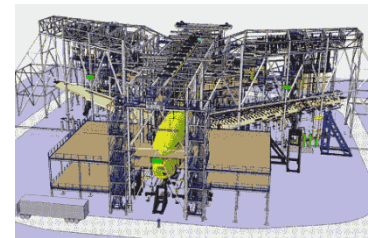
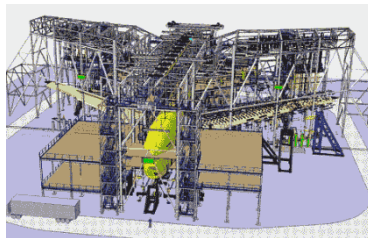
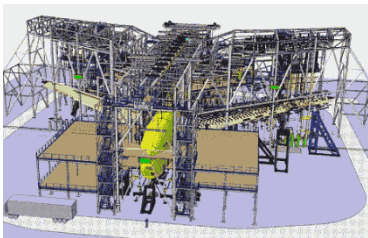
Even among component parts, mixed material:
How to test hybrid junctions



- Cost & Time saving:

2 Fatigue Cells (Metal +CFRP)

1 Hybrid Fatigue Cell



Hybrid Fatigue Full scale Cells ?

Current scenarios:

Metal test scenario

Fatigue sensitive areas:
all stress concentration areas

Fatigue mainly driven by local
tension loading $R=0.1$

Scatter covered by Test Life
factor : 2 ...3



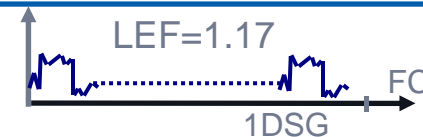
Composite test scenario

Fatigue sensitive features:
Feature with out-of-plane stresses
Shear and Tensile inter lamina strength

Compression: Mainly driven by
compression and alternative
loading $R=-1$

Scatter covered by LEF Load
Enhancement Factor: 1.17*

*from Northrop approach



Hybrid Fatigue Full scale Cells ?

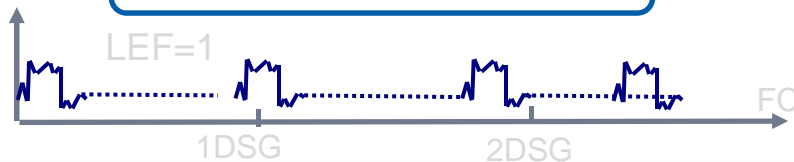
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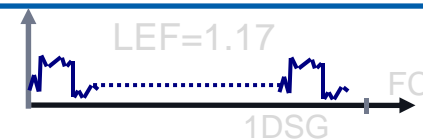
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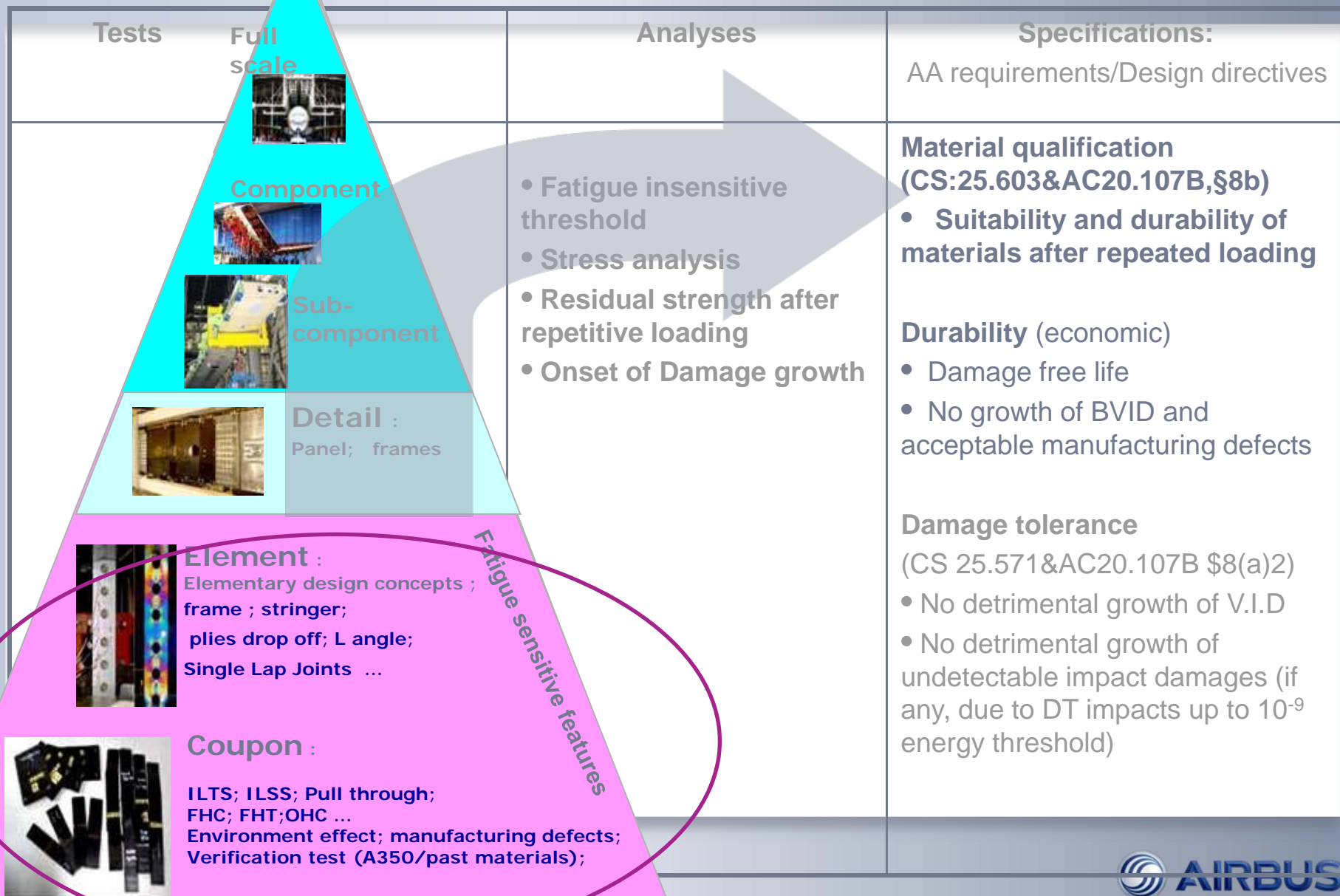
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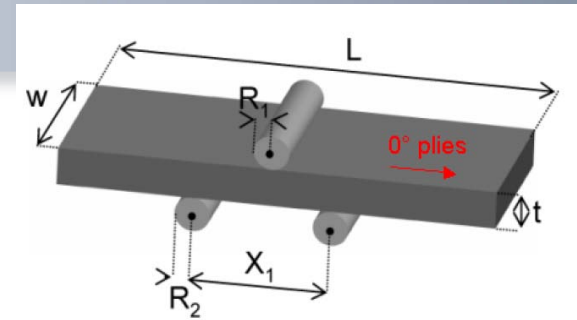
Composite Test pyramid

Tests / Analyses / Specifications

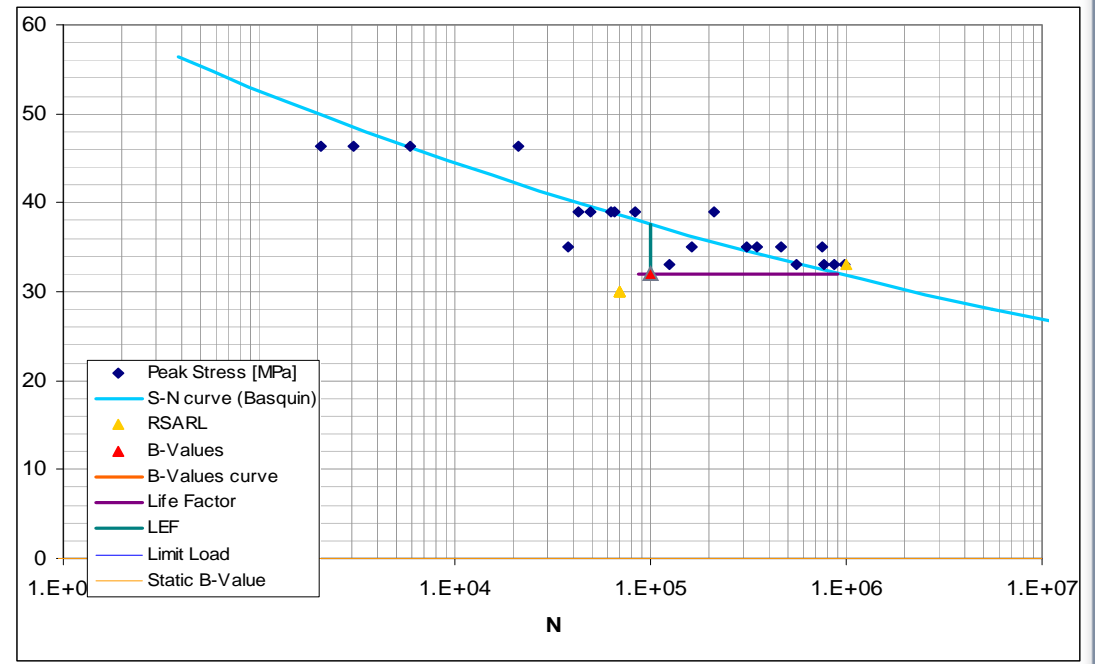
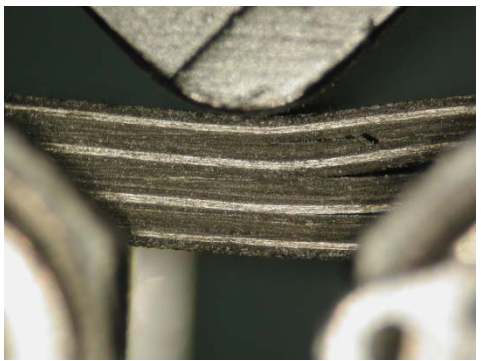


Fatigue method for composite: Wöhler curve

- Fatigue sensitive feature :
- Example : Inter Laminar Shear Stress Test
- $t=4\text{mm}$, $W=15$, $L=40\text{mm}$ $X=20$



$$N=C(|\sigma_{max}|)^{-m}$$



Failure/Residual strength/B values

➔ Fatigue features sensitivity drive the design principle

LEF definition

Load Enhancement Factor has been introduced on fatigue composite full scale test as a response to the higher scatter observed on fatigue composite tests

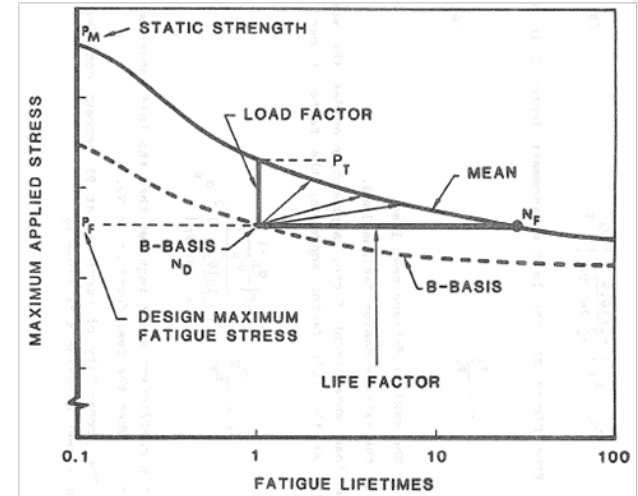
Composite standard approach:

1986-Northrop's report proposed a 2 parameters Weibull law analysis.

Resulting from a large number of coupon tests,

| | | | | |
|-----|-------|-------|------|------|
| N | 1 | 1.5 | 3 | 13.3 |
| LEF | 1.177 | 1.148 | 1.10 | 1 |

Remarks : Test campaign with all failure mode (not focused on sizing criteria)



$$LEF = \left(\frac{N_F}{N} \right)^{\alpha_R}$$

$$N_F = \frac{\Gamma \left(\frac{\alpha_L + 1}{\alpha_L} \right)}{\left[\frac{-\ln(p)}{\chi^2_{\gamma}(2n) / 2n} \right]^{\frac{1}{\alpha_L}}}$$

- N_F is the resulting life factor for LEF=1
- α_R Weibull shape parameter for the scatter on residual strength properties
- α_L Weibull shape parameter for the scatter on fatigue life properties
- p Survival probability (90% for the B-value definition)
- g Confidence (95%)
- N Coefficient applied on the life (N = Life Factor when LEF = 1)
- n Number of test articles (usually one for a full-scale test)

LEF definition (con't)

Other analyses:

$$N_F = \frac{\Gamma\left(\frac{\alpha_L+1}{\alpha_L}\right)}{\left[\frac{-\ln(p)}{\chi^2_\gamma(2n)/2n}\right]^{\frac{1}{\alpha_L}}} \quad \text{LEF} = \left(\frac{N_F}{N}\right)^{\frac{\alpha_L}{\alpha_R}}$$

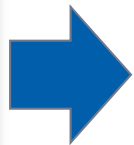
| | Inputs | | Outputs | | | |
|----------------------|---------|---------|------------|--------------|------------|------------|
| | Alpha R | Alpha L | LEF (1DSG) | LEF (1.5DSG) | LEF (3DSG) | Nf (LEF=1) |
| Northrop 1986 | 20,00 | 1,25 | 1,177 | 1,15 | 1,10 | 13,56 |
| EADS ATR 1989 | | | 1,10 | | | 5,13 |
| EADS CASA 2001 | 19,86 | 2,74 | 1,16 | 1,10 | 1,00 | 3,02 |
| NIAR 2008 AS4/E7K8 | 24,23 | 1,74 | 1,14 | 1,11 | 1,05 | 6,09 |
| NIAR 2008 T700 | 34,58 | 4,06 | 1,09 | 1,04 | 0,96 | 2,07 |
| Airbus 2011 FatSensF | 24,20 | 2,31 | 1,14 | 1,09 | 1,02 | 3,78 |

LEF Trends versus (α_R, α_L)

$\alpha_R \nearrow \Rightarrow \text{LEF}(1\text{DSG}) \searrow$
 \Rightarrow but static scatter \searrow

$\alpha_L \nearrow \Rightarrow \text{LEF}(3\text{DSG}) \searrow$

| | Alpha R | Alpha L | LEF (1DSG) | LEF (1.5DSG) | LEF (3DSG) | Nf (LEF=1) | Coef Variance |
|---------------|---------|---------|------------|--------------|------------|------------|---------------|
| | 10 | 1,25 | 1,385 | 1,32 | 1,21 | 13,56 | 12,03 |
| Northrop 1986 | 20 | 1,25 | 1,177 | 1,15 | 1,10 | 13,56 | 6,20 |
| | 30 | 1,25 | 1,115 | 1,10 | 1,06 | 13,56 | 4,18 |
| | 40 | 1,25 | 1,085 | 1,07 | 1,05 | 13,56 | 3,15 |
| | 50 | 1,25 | 1,067 | 1,06 | 1,04 | 13,56 | 2,53 |
| Northrop 1986 | 20,00 | 1,25 | 1,177 | 1,15 | 1,10 | 13,56 | 6,20 |
| | 20 | 2 | 1,168 | 1,12 | 1,05 | 4,73 | 6,20 |
| | 20 | 4 | 1,159 | 1,07 | 0,93 | 2,09 | 6,20 |



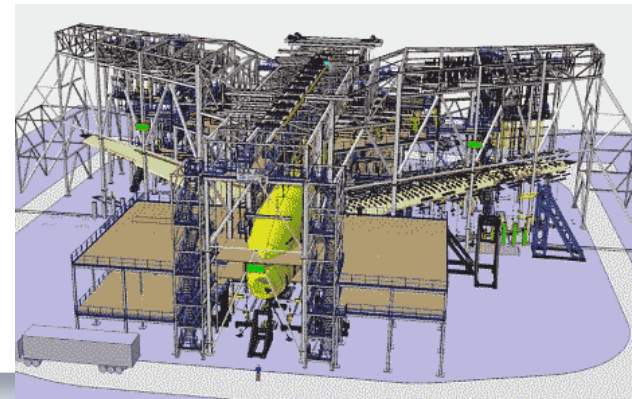
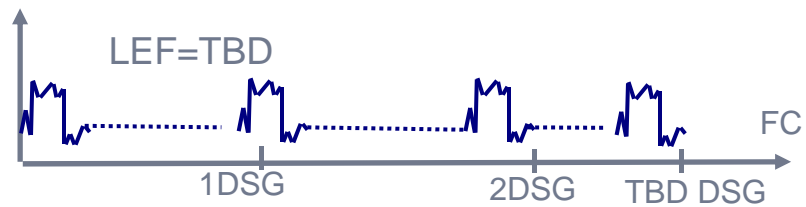
- challenge LEF(1DSG)~1.17 quite ambitious versus Material variance
- opportunity to decrease LEF (2, or 3DSG)

Hybrid Test scenario

Factor to be adjusted

- LEF=1.0 up to 1.05
- Life Factor 2..3 DSG

Adapted scenario



Perspectives

Pre requisite on LEF identification

- Wide materials/process used world wide
- Large population of coupons tests needed
- Set test means

Set the standards of LEF definition

- Pool only fatigue sensitive features
- Define the categories of failure that set up same phenomenon:
disbonding; delamination; impacted damage growth, max strength
....
- Justification of Weibull 2 factors analysis

=> Pool one's results upon standards



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